

SIGNIFICANCE OF SURFACE PRE-TREATMENT FOR DIFFERENT CUTTING TOOLS COTED BY CA-PHYSICAL VAPOUR DEPOSITION

AnilKrishna.Battu¹, K.I.V.Vandana², K.SivajiBabu³

^{1,2,3}Department of Mechanical Engineering (Machine Design), PVPSIT, Kanuru, Vijayawada

ABSTRACT: With the advent of new materials with high performance to meet the current applications has increased the complexity in machining because of their high strength, hardness, toughness. Two widely accepted solutions are there to overcome this problem which is hard metals and surface coatings. In coatings physical vapour deposition technology and chemical vapour deposition technology had used on cutting tools to machine these types of materials. Even though there are some problems like rapid tool wear and/or abnormal tool failure occurred because of poor adhesion, high surface roughness value and sharp cutting edges of the cutting tools. To eliminate these difficulties, pre-treatment technique is one of the viable solution and also to enhance the tool life further. Micro-blasting on PVD films has been documented, among others, as an efficient method for inducing compressive stresses, thus for increasing the coating hardness and potentially tool life of coated tools. Since contradictory results have been registered concerning the efficiency of wet micro-blasting on coated tools for improving the wear behavior, the paper aims at explaining how this process can be successfully applied for post-treatment of PVD films. In this context, the employed conditions such as pressure and grain size affects significantly the wear resistance of the micro-blasted coated tools.

1. INTRODUCTION

Now a days machining is one of the major operation which is widely carrying out in many industries such as automobile, aerospace, locomotive, marine, etc. The main objective in the machining operations like drilling, boring, milling, reaming, turning, etc. is to transform a raw material into specific desired shape. While in the transformation cutting tool had a prominent role. Therefore, tool life is the main criterion which decides productivity of machining operation. But there are many changes had occurred in materials to suit with current applications. Traditional materials would not be suitable for this purpose so, now a days industries using advanced exotic materials like composites, hard powder metals, bimetal, high strength alloys, Inconel, carbon fiber reinforced plastic, etc. Despite to the advancement in materials, the machining operation had become very difficult and simultaneously tool life was also decreases rapidly. Because, while performing the machining operations there would be a chance of high temperature, stresses and forces generation at contact point between the cutting tool and material and also rapid tool wear was taking place.

So, surface treatment technique had a possible solution to avoid these difficulties. This can be done by applying a layer of film or coating onto the existing surface to create a new surface with altering the base material properties. Chemical Vapour Deposition (CVD) and Physical Vapour Deposition (PVD) are the two most prominent coating process treatments. PVD process had been widely using coating treatment than CVD.

Despite to this process treatment rapid tool wear and failure are still major problems in all machining processes. Tool wear such as flank wear, corner wear and built up edge could effects hole quality and surface finish of the product. Thus, besides the coating material properties and specifications a large number of further parameters affect the coating performance in cutting tool applications. So, along with the coating technique, cutting edge geometry and surface pre-treatment technique had also placed a vital role in hard machining and high speed machining.

2. TWIST DRILL BIT GEOMETRY

Drilling is one of the most commonly used machining processes. A typical drill has several design parameters such as tip angle, chisel edge angle, chisel edge length, cutting lip length and helix angle. It is known

that a drill consists of two main cutting edges, namely; the chisel edge and the cutting lips. The Chisel edge extrudes into the work piece material and contributes substantially to the thrust force. The cutting lips cut out the material and produce the majority of the drilling torque. [1]. The drill geometry influences the cutting force effects on the tool and additionally material properties of tool and workpiece along with machining conditions also influences the cutting forces.

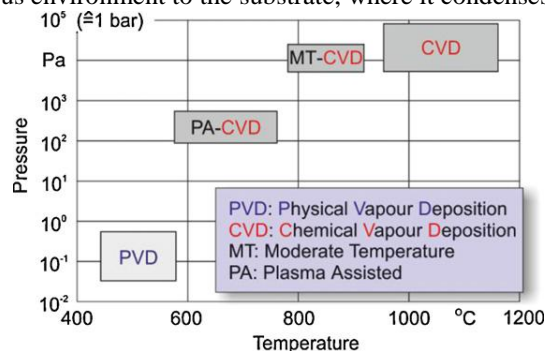
Twist drills: In the case of drilling, the new developments are mainly relates to

- Drill point geometry has to be improved for better results.
- Materials and coatings are used to improve the performance and tool life.

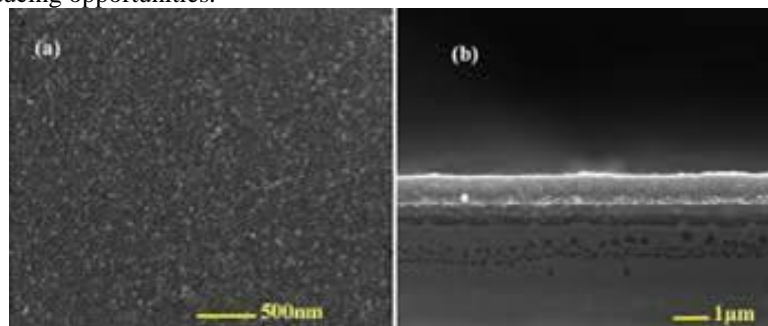
3. THIN FILM DEPOSITION

Surface engineering involves changing the properties of the surface and near surface region in a desirable way. Surface engineering involves an overlay process or surface modification process. In overlay process a material is added to the surface and the underlying material is covered and not detectable on the surface. This process changes the properties of the substrate but the surface material is still present on the surface.

Physical Vapour Deposition (PVD) is one of the most prominent processes which were used in the thin film deposition techniques. PVD processes are atomistic deposition processes in which material is vaporized from a solid or liquid source in the form of atoms or molecules and transported in the form of a vapour through vacuum or low pressure gaseous environment to the substrate, where it condenses [2].



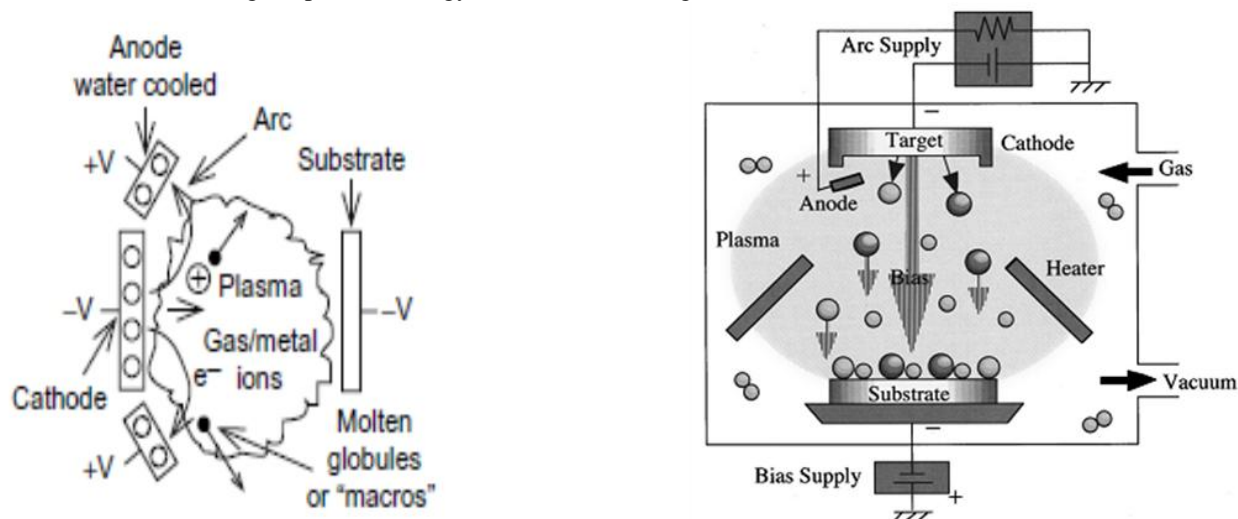
CVD coatings were already commercialized for carbide inserts in the 1960s. PVD was developed almost 20 years later and today both CVD and PVD are sharing the coating market of cutting tools. PVD coatings for cutting tools can be deposited at temperatures lying in the range of 450°C to 550°C, which allows the film deposition on high speed steel tools. Moreover the ability to control thickness on the edges, when PVD is employed, guarantees a sharp coated edge. PVD films can be produced without any chemical interaction with the substrate. CVD coatings easily interact with the substrates, occasionally producing brittle carbides at the interfaces. The ease of decoating and resharpenering of PVD coated tools opened a large industrial market highly sensitive to cost reducing opportunities.



3.1 CATHODIC ARC

Cathodic arc deposition or Arc-PVD is a physical vapor deposition technique in which an electric arc is used to vaporize material from a cathode target. The vaporized material then made to condense on a substrate to form a film. In this method, a small limited area (few microns) is evaporated with a very high-energy arc that quickly moves over the metal surface to be evaporated. The plasma generated consists of highly ionized metal

vapor (approx. 50 – 100%). The ionization rate is considerably greater than any other process of PVD. The energy associated with the evaporated species during the deposition of coating depends on the bias voltage given to the substrate (the component on which one is interested to coat), which is also responsible for control of momentum transfer. The amount of momentum transfer is highest in the case of the cathodic arc deposition process. This leads to high deposition energy, and a dense coating [2].



4. TYPE OF COATINGS

4.1 TiN, the first universal coating

A number of different hard coatings, binary, ternary and quaternary compositions were deposited by CVAE in the former Soviet Union [4,5,6], but in the West mostly TiN coatings have been deposited using different PVD techniques. Therefore it is no surprise, that we can find successful TiN coatings in all fields of applications. However, for most applications we can also choose another coating which is similar or better performance than TiN. It is interesting to report the results on tools for sewing needle manufacture and the sewing needles themselves which are coated at 200°C. Replacing hard chrome with TiN significantly increases the lifetime of the needles.

4.2 CrN, the second universal coating

The fine grained coating combines low brittleness and sufficient hardness with good oxidation resistance and chemical inertness. Industrial experience shows that the CrN coatings can perform better in metal forming than the CVD TiC/TiN coating. The lifetime of CrN tools increased by a factor greater than 30. CrN coatings also show very good results in manufacturing copper materials both forming and cutting and when cutting turbine blade materials (Inconel) as well as in glass forming. Moulds for parts made of elastomers, thermoplastics and phenol plastics have been coated successfully for many years. It was also found that CrN coatings increase the lifetime of mould broaches in die casting of aluminium in the range of a factor of 2-15.

4.3 (Al, Ti)N, a high oxidation resistant coating

It is well known that higher cutting speeds as well as "bad" lubrication conditions are connected with the generation of high temperatures. (Al,Ti)N coatings with a high Al-content (metal content $[Al]/[Ti] > 1$) are the most oxidation resistant coatings deposited by the CVAE process onto tools [7]. So this coating is the best candidate to meet the conditions of high cutting speeds and "unlubricated" operation. However, it was reported that (Ti,Al)N coatings (metal content $[Al]/[Ti] = 1$) deposited by magnetron sputtering are not suitable for milling operations [8]. AlTiN coatings deposited by CVAE can increase significantly the performance of milling tools. Excellent results were obtained in the cutting of high nickel-alloyed materials and of grey cast iron. It was also reported that for the forming of non-ferrous materials such as high-nickel alloys or titanium alloys, AlTiN coatings can perform better than the other coatings.

4.4 Other coatings

It is possible to increase the hardness or the oxidation resistance of titanium-based coatings by alloying with Zr, Nb, Hf, V, W and B [5,10,6,7,10,11]. These coatings have application niches where they show

better performance than the other coatings. CrCN coatings are successfully applied for plastic tools and different cutting operations.

4.5 Combined coatings

For some applications, combination coatings are more effective than PVD coatings alone. In the specific case of tribological systems with corrosive action, the combination of an electroless nickel layer with a PVD coating should be applied. Another important variant is the combination of nitriding treatment with the deposition of a hard coating. This allows the load-bearing capacity of the composite to be raised and also gives a wear reserve. Initially, results of coating CVD-coated hard metal inserts with PVD coatings showed the possibility of an increase in lifetime [7].

5. SIGNIFICANCE OF PRE-TREATMENT

As per the literature review, pre-treatment for different cutting tools before coating would affect the tool performance. Previous researchers explained the significance of different surface pre-treatment, post-treatment for different type of coatings and also explained the effects of it.

- **C. Subramanian et al.** 2 μ m thick TiN coatings were deposited on M2 HSS twist drills, coated and uncoated bits were tested and SEM studies carried out to explain the possible wear mechanism. Was able to estimate, Compared to bare TiN performs 4 times better
- **R. Buhl et al.** studied in detail the PVD deposited TiN for microstructure, adhesion and machining properties. Also gave a 4 times higher life to TiN coated tools when compared to bare
- **W. D Sproul et al.** compared PVD coated and sputtered TiN bits with and without coolant, finally giving a life 20-30 times more than bare bit
- **S.G Harris et al.** influence of chromium content was studied in TiAlN coatings. An improvement in tool life was observed based on Cr addition.
- **K.-D. Bouzakis et al.** Micro blasting on pvd films has been documented as a potentially efficient method for improving the cutting performance of coated tools. This process induces residual compressive stresses into the film structure, thus increasing the coating hardness but its brittleness too. Micro blasting parameters pressure and time have crucial effect on the coated tools cutting performance. Along with this Bouzakis also investigated the potential for increasing the wear resistance of PVD TiAlN coated cemented carbide tools through wet micro-blasting by Al_2O_3 abrasive grains of different diameters. The grain size is pivotal for the developed hardness and residual stresses close to the film surface and for the cutting edge integrity as well. Herewith, the wear resistance of coated tools can be significantly improved.
- **Knotek et al.** state that coating adhesion increases with improved surface quality and surfaces with low roughness values offer more favorable growth conditions for hard PVD films, increasing micro-hardness and coating rate (speed of growth of the coating thickness during the PVD process)
- **S.G Harris et al.** influence of chromium content was studied in TiAlN coatings. An improvement in tool life was observed based on Cr addition.
- **Bouzakis et al.** applied micro-blasting to cemented tungsten carbide inserts and observed that Co is removed from the surface to be coated. Moreover, high roughness peaks are reduced due to the removal of carbide grains and numerous new smaller peaks are revealed, thus contributing to the enhancement of substrate-coating adhesion. The increased coating adhesion occurs due to the better mechanical binding of the deposited coating on the substrate surface through small roughness peaks.
- **B. Denkena et al** Coating adhesion is dependent on the surface roughness of the prepared inserts and on the difference between residual stresses in the coating and in the substrate near the interface. Higher compressive residual stresses on the substrate after coating contribute to the decrease of tool wear, since the rupture of the insert material is hindered. Since the coating is rapidly removed, the properties of the substrate have a great influence on insert performance.

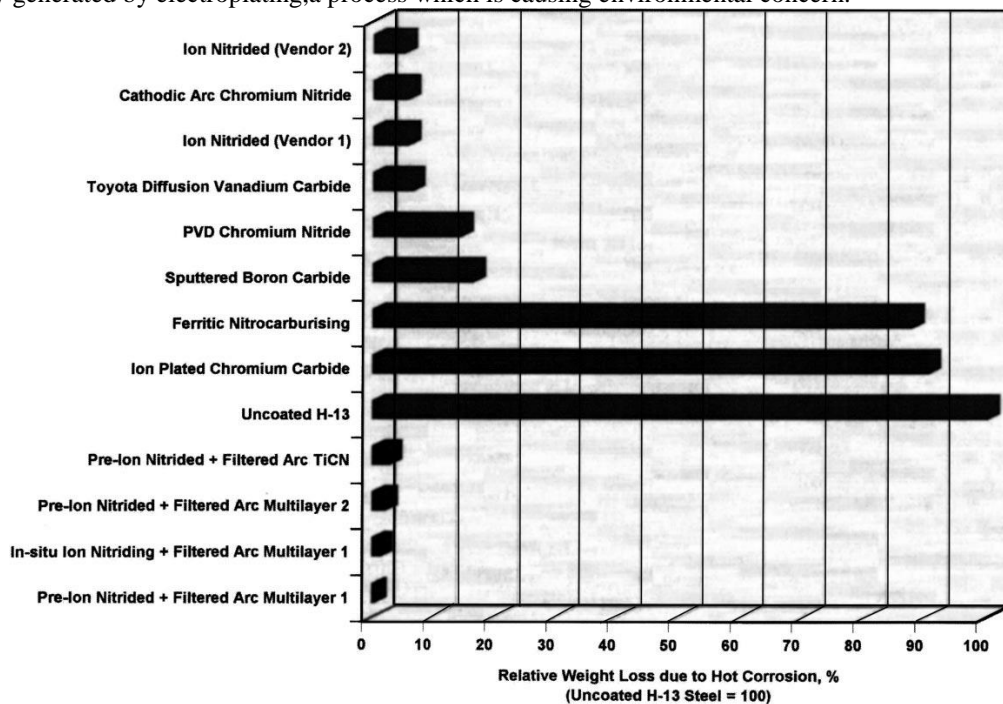
6. EMERGING APPLICATIONS

As mentioned earlier, the major commercial application for cathodic arc technology is in the enhancement of useful life for cutting tools with 7x. This is likely the case because major benefits in tool life were achieved despite the presence of macroparticles in the coatings. With the advent of commercially available arc filters, we expect to see new applications which depend on being able to produce macroparticle-free

coatings. While many of these applications are still tightly protected trade secrets, we have listed some examples below which have been reported in the open literature.

6.1 Example: corrosion protection of dies

Figure shows a comparison of the corrosion behavior of some die pins which have been given a variety of different surface treatments and subsequently exposed to molten aluminum. The sample which was pre-nitrided and subsequently coated with a TiN/TiBCN multilayer coating prepared in the filtered cathodic arc system, showed virtually no corrosion in this hostile environment [24]. Once again, this application requires filtering of the arc since macroparticles in the coating would provide a path for the corrosive medium to gain access to the underlying part. The demonstrated success of filtered arc multilayer coatings for corrosion protection suggests additional applications may become practical such as the replacement of chromium coatings currently generated by electroplating, a process which is causing environmental concern.



Comparison of corrosion resistance of die pins treated with various surface treatments, the most successful being a duplex coating with a filtered-arc-produced TiN/TiBCN multilayer coating [24]. Courtesy of D. Bhat.

6.2 Example: hard carbon films

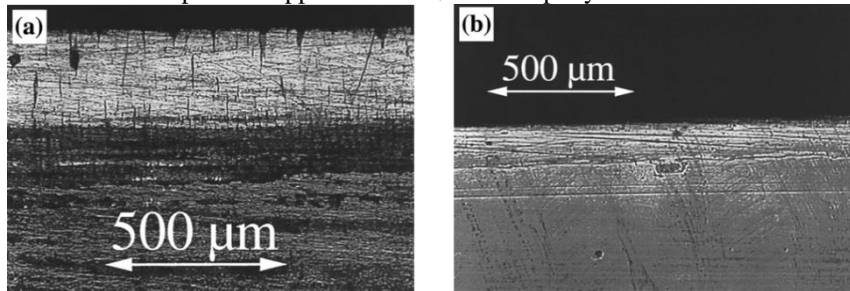
As discussed earlier, cathodic arc deposited carbon is a particularly interesting system because of the wide variety of coating structures and morphologies which can be generated. Potential applications for coatings produced by a filtered arc abound. It has been suggested that they may have value in protecting knife edges and surgical blades since extremely hard smooth coatings are possible. They may prove useful for bearing surfaces in high precision machine tools for the same reason [25,26]. Electron emissive carbon coatings [27] suitable for flat panel displays have been demonstrated [28,29], and electron emission from vacuum-arc a-C coated nanotubes is being investigated [30].

Cathodic arc systems with advanced filters such as the Twist Filter may represent a possible avenue for synthesizing ultrathin films having the required features. However, pulsed-arc synthesized carbon films can be very hard and elastic even when sp^2 bonds dominate, provided the graphene sheets are curved [31]. The range of carbon-based materials is still growing and we should be prepared to see more interesting properties discovered in this field.

6.3 Example: nitrides, oxides, carbides and other coatings

Unfiltered cathodic arc deposition of TiN coatings is a well-established technology [33,34] which supports tens of millions of dollars of business annually worldwide in coating equipment sales and hundreds of millions of dollars annually for the coatings generated by that equipment [32]. Most of the arc-TiN coatings

are decorative and protective coatings on plumbing fixtures, door knobs and lamp reflectors. Welty estimates that the value of cathodic-arc-coated products approaches US\$1 billion per year.



Comparison of thermal fatigue behavior of coated and un-coated H13 steel die pins (a) Optical micrograph of an uncoated pin; (b) TiN/TiBCN multilayer-coated pin. The multilayer produced in the filtered cathodic arc system prevents surface cracking that is found in the uncoated part. Courtesy of D. Bhat.

The reason that the industry can use the reactive arc deposition process for these applications is the technologists have learned to diminish the quantity of macroparticles by making thinner coatings, using appropriate side shielding and magnetic fields.

7. SUMMARY AND OUTLOOK

Although cathodic arc deposition is one of the earliest plasma technologies, its commercial use has been largely limited to applications where some number of macroparticles can be tolerated such as lifetime extension of machine tools and decorative applications such as plumbing fixtures, and door knobs. Recent progress in the development of macroparticle filters is likely to extend this list of applications. The driving force to pursue arc technology, as opposed to evaporation and sputtering technologies are the often outstanding properties of the films deposited, and the wider process window (range of partial pressure) in reactive plasma deposition. Film properties can be readily tuned and tailored because cathodic arc plasmas are fully ionized. With the introduction of the improved ability to control the arc trajectory and plasma trajectory, it is likely a larger range of applications will be pursued. The productivity increase demands in cutting processes can be addressed, among others, through the application of coated tools. The paper deals at first with current trends of coated tools manufacturing, providing an overview on the evolution of film deposition technologies, coating materials and adhesive interlayers. Moreover, coated tools wear mechanisms were explained by innovative methods for characterizing film material, functional and dimensional properties. These issues are supported by sophisticated computational procedures, which contribute in obtaining a thorough understanding of the tool wear mechanism taking place during cutting with coated tools. The described procedures allow the prediction of coated tool cutting performance and the effective adaption of the cutting conditions to the film properties, thus restricting the related experimental cost. Appropriate substrate and coating thermal as well as mechanical treatments improving the tool wear behavior, were also introduced. The potential of applying coated cutting tools in difficult-to-cut materials was exhibited in characteristic workpiece material cases. Finally, the possibility of reconditioning worn coated solid cutting tools and its effect on the mechanical properties, the cutting edge sharpness and performance was highlighted.

REFERENCES

- [1]. M. Pirtini, I. Lazoglu, Forces and hole quality in drilling, *International Journal of Machine Tools & Manufacture* 45 (2005) 1271–1281.
- [2]. Handbook Physical Vapour Deposition
- [3]. S.S. Icharkov, T.A. Chodakova, V.G. Lapteva, A.A. Andreev and I.V. Gavrilko, *Trakt. Sel'khoz mashiny*, 6 (1978) 37.
- [4]. A.A. Andreev, I.V. Gavrilko, A.G. Gavrilov, A.S. Veretsaka, V.P. Zed, V.P. Padalka, A.K. Karlovic and V.T. Tolok, *DE* 3152742, 1983.
- [5]. A.S. Veretschaka, *Performance of Cutting Tools with Wear Protecting Coatings*, Maschinostroenie, Moscow, 1993,
- [6]. T. Ikeda and H. Satoh, *Thin Solid Films*, 195 (1991) 99.
- [7]. W. König and D. Kammermeier, *Industrie-Anzeiger*, 43 (1991) 80.
- [8]. J. Vetter, H.J. Schöli and O. Knotek, TiCrN coatings deposited by cathodic vacuum arc evaporation, *Surf. Coat. Technol.*, 74-75 (1995) 286.

- [9]. Information, OMT, Lt-beck.
- [10]. O. Knotek, M. B/Shiner, F. L&fter, R. BreidenbachandC. StOssel, Metall, 46 (1992) 234.
- [11]. K.D.Bouzakis, G.Skordaris, S.Gerardis, G.Katirtzoglou, S.Makrimalakis, M.Pappa, S.Bolz, W.Koelker, The effect of substrate pretreatments and HPPMS-deposited adhesive interlayers materials on the cutting performance of coated cemented carbide inserts, CIRP Annals - Manufacturing Technology 59 (2010) 73–76
- [12]. B. Denkena, A. Lucas, E. Bassett, Effects of the cutting edge microgeometry on tool wear and its thermo mechanical load, CIRP Annals - Manufacturing Technology 60 (2011) 73–76.
- [13]. B.Denkena, D. Biermann, cutting edge geometries, CIRP Annals-Manufacturing Technology 63 (2014) 631-653.
- [14]. B. Denkena, J. Köhler, B. Breidenstein, A.M. Abrao, C.E.H. Ventura, Influence of the cutting edge preparation method on characteristics and performance of PVD coated carbide inserts in hard turning, Surface & Coatings Technology 254 (2014) 447–454
- [15]. K.-D. Bouzakis, N. Michailidis, S.Hadjiyiannis, K. Efstathiou, E. Pavlidou, G. Erkens, S. Rambadt, I. Wirth, Improvement of PVD coated inserts cutting performance, through appropriate mechanical treatments of substrate and coating surface, Surface and Coatings Technology 146–147 (2001) 443–450.
- [16]. K.Narasimhan, S.P.Boppana, D.G.Bhat, Development of a graded TiCN coating for cemented carbide cutting tools—a design approach, Wear188(1–2)(1995)123–129
- [17]. O. Knotek, F. Löffler and G. Kramer, Substrate- and interface-related influences on the performance of arc physical- vapour-deposition-coated cemented carbides in interrupted-cut machining, Surface and Coatings Technology, 54/55 (1992) 476-481.
- [18]. Krishnan Narasimhan, S. Prasad Boppana, Deepak G. Bhat, Development of a graded TiCN coating for cemented carbide cutting tools-a design approach, Wear 188 (1995) 123-129.
- [19]. S.G. Harris a,*, E.D. Doyle a, A.C. Vlasveld a, J. Audya, D. Quick b, A study of the wear mechanisms of Ti1–xAlxN and Ti1–x–yAlxCrN coated high-speed steel twist drills under dry machining conditions, Wear 254 (2003) 723–734
- [20]. A. Ho`rlinga, L. Hultman, M. Oden, J. Sjolen, L. Karlsson, Mechanical properties and machining performance of Ti1 xAlxN-coated cutting tools, Surface & Coatings Technology 191 (2005) 384– 392
- [21]. J. Vetter, Vacuum arc coatings for tools: potential and application, Surface and Coatings Technology 76-77 (1995) 719-724.
- [22]. Krishna Valleti , C. Rejin, Shrikant V. Joshi, Factors influencing properties of CrN thin films grown by cylindrical cathodic arc physical vapor deposition on HSS substrates, Materials Science and Engineering A 545 (2012) 155– 161
- [23]. D.G. Bhat, V. Gorokhovskiy, R. Bhattacharya, R. Shivpuri, Development of a Coating for Wear and Cracking Prevention in Die-casting Dies by the Filtered Cathodic Arc Process, NADCA Int. Die Casting Congress, Cleveland, OH, 1999, Paper T99-112.
- [24]. T. Witke, T. Schuelke, J. Berthold, C.F. Meyer, B. Schultrich,
- [25]. Surf. Coat. Technol. 116-119 (1999) 609-613.
- [26]. B. Schultrich, H.J. Scheibe, D. Drescher, H. Ziegele, Surf.Coat. Technol. 98(1998).1097-1101.
- [27]. A.V. Karabutov, V.I. Konov, V.G. Ralchenko et al., Diam.Relat. Materials 7 (1998) 802-806.
- [28]. B.F. Coll, J. Jaskie, J. Markham, E. Menu, A. Talin, Preparation of disordered amorphous and partially ordered nano clustered carbon films by arc deposition: a critical review, in: S.R.P. Silva, J. Robertson, W.I. Milne, and G.A.J. Amaratunga Eds., Proceedings of the 1st International Specialist Meeting on Amorphous Carbon SMAC'97., Cambridge, UK, 31 July-1Aug. 1997, Singapore World Scientific, 1998, pp. 91-116.
- [29]. B.F. Coll, J.E. Jaskie, J.L. Markham, E.P. Menu, A.A. Talin, P. Von Allmen, Field emission properties of disordered and partially ordered nano clustered carbon films, in: M.P. Siegal, W.I. Milne, J.E. Jaskie Eds., Materials Research Society Proceedings, Symposium on Covalently Bonded Disordered Thin-Film Materials, Boston, MA, 2-4 Dec. 1997, MRS, Warrendale, PA, 1998, pp. 185-196.
- [30]. S. Dimitrijevic, J.C. Withers, V. Mammana, O.R. Monteiro, J.W. Ager III, I.G. Brown, Appl. Phys. Lett. 75 (1999) 2680-2682.
- [31]. G. Vergason, Personal Communication, 2000
- [32]. B.K. Tay, X. Shi, H.S. Yang, H.S. Tan, D. Chua, S.Y. Teo, Surf. Coat. Technol. 111 (1999) 229-233.
- [33]. P.J. Martin, A. Bendavid, T.J. Kinder, L. Wielunski, Surf.Coat. Technol. 87 (1996) 271-278.